



**AERC 2009**

**5th Annual European Rheology Conference**

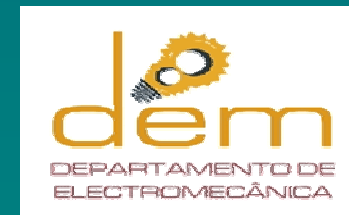
**April 15-17, Cardiff - United Kingdom**

# **Unsteady Viscoelastic Flow in a Planar “T” Junction**

***Helder M. Matos , Paulo J. Oliveira***

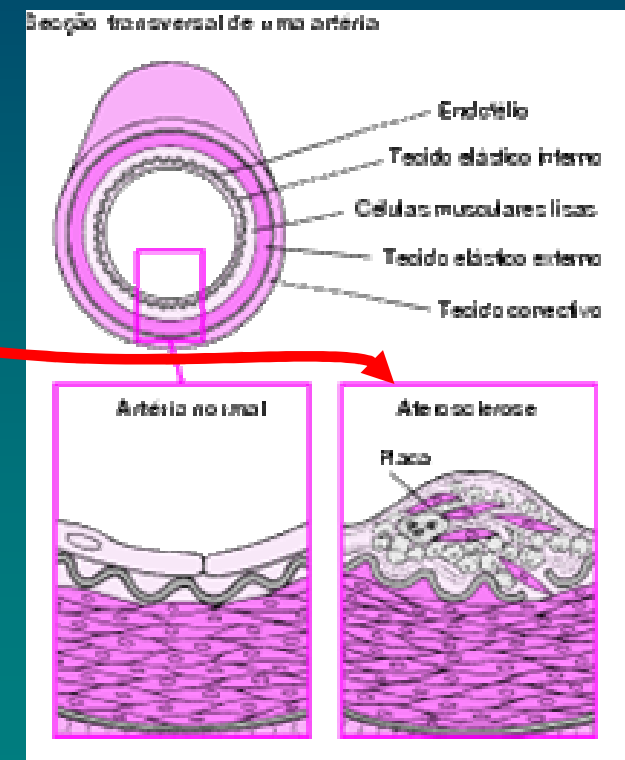
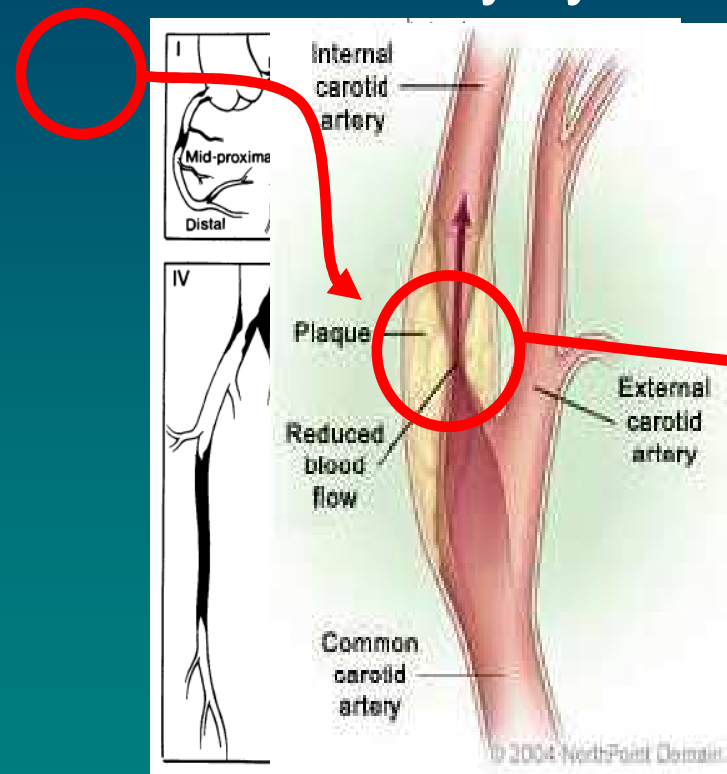


**Universidade da  
Beira  
Interior**



# 1 - T-JUNCTION FLOWS (test case)

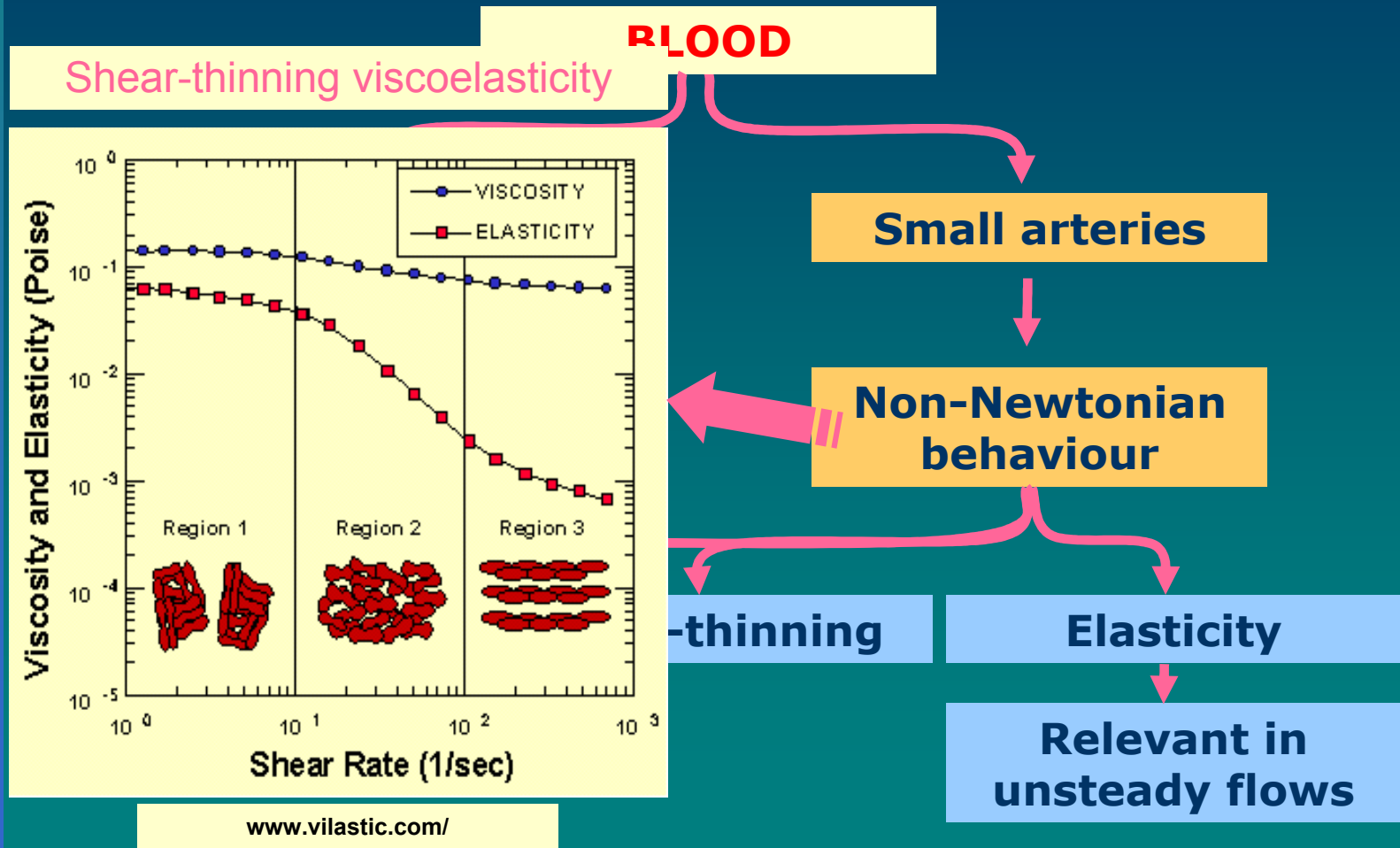
## ■ The human circulatory system



Del [www.tcg.cardiologydomain.com/](http://www.tcg.cardiologydomain.com/)  
*Ann Surg.* 201(2), 115–131.

[www.manualmerck.net/](http://www.manualmerck.net/)

## 2 - RHEOLOGY OF BLOOD



# 3 - OBJECTIVES

- Investigate unsteady flow through a 2D bifurcation using a viscoelastic fluid model (FENE CR: Constant viscosity).
- First approach to blood flow simulations (elasticity usually neglected).
- Evaluate influence of flow rate ratio ( $\beta$ ) and elasticity (Deborah number (De), at constant extensibility ( $L^2$ ) and polymer concentration (c)).

$$De = \frac{\lambda u_1}{H}$$

$$0 \leq De \leq 10$$

$$c = \frac{\eta_P}{\eta_S} = 0.11$$

$$\eta_0 = \eta_S + \eta_P$$

$$\beta = \frac{Q_3}{Q_1}$$

$$0.1 \leq \beta \leq 0.9$$

$$L^2 = 100$$

# 4 - EQUATIONS

- Conservation of mass

$$\nabla \cdot \mathbf{u} = 0$$

- Conservation of linear momentum

$$\rho \frac{D\mathbf{u}}{Dt} = -\nabla p + \nabla \cdot \boldsymbol{\tau} + \nabla \cdot (\eta_s \mathbf{D})$$

- Constitutive equation

- FENE CR Model

(Chilcott e Rallison, 1988)

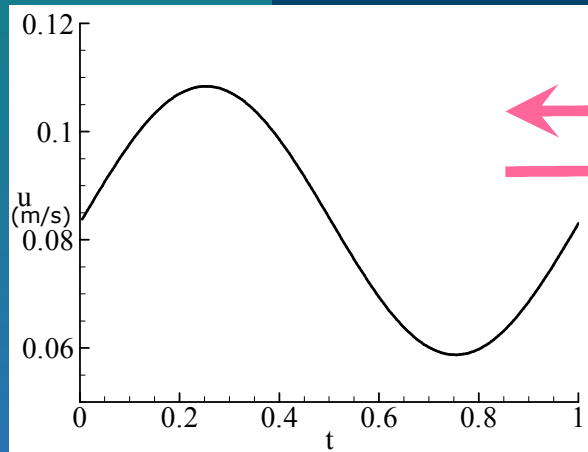
$$\boldsymbol{\tau} + \lambda \left( \frac{\nabla \cdot \boldsymbol{\tau}}{f(\boldsymbol{\tau})} \right) = 2\eta_p \mathbf{D}$$

$$f(\boldsymbol{\tau}) = \frac{L^2 + (\lambda / \eta_p) \text{tr}(\boldsymbol{\tau})}{L^2 - 3}$$

# 5 - NUMERICAL PROCEDURE

- Finite-volume method for discretization of equations.
- Nonstaggered mesh arrangement.
  - Pressure-velocity coupling: Rhie & Chow, 1983.
  - Stress-velocity coupling: Oliveira et al., 1999.
- Spatial discretisation (convective terms): CUBISTA scheme (Alves et al. 2003).
- Temporal discretisation (unsteady term): Three-time level scheme (Oliveira 2001).
- Pressure-correction: SIMPLEC algorithm with time-marching.

# 6 - FLOW GEOMETRY



Miranda, A.I.P., et al. (2008), Int. J. Numer. Meth. Fluids, 57, 295-328.

Generated by an sinusoidal pressure gradient

$$-\frac{dp}{dx} = \rho K_s + \rho K_0 \cos(\omega t)$$

$$\rho K_s = 75.1 \text{ Pa/m}$$

$$\rho K_0 = 190 \text{ Pa/m}$$

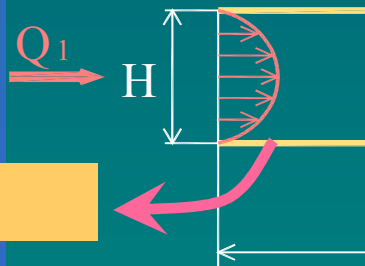
$$\omega = 2\pi f = 2.2\pi \text{ s}^{-1}$$

$$K_0 / K_s = 2.53$$

$$T = 0.91 \text{ s}$$

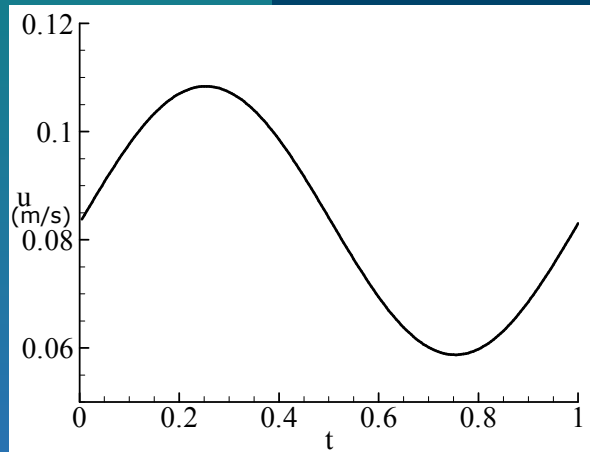
Womersley number

$$\alpha = \left[ \frac{H}{2} \cdot \left( \frac{\omega}{\nu} \right)^{1/2} \right] = 4.864$$

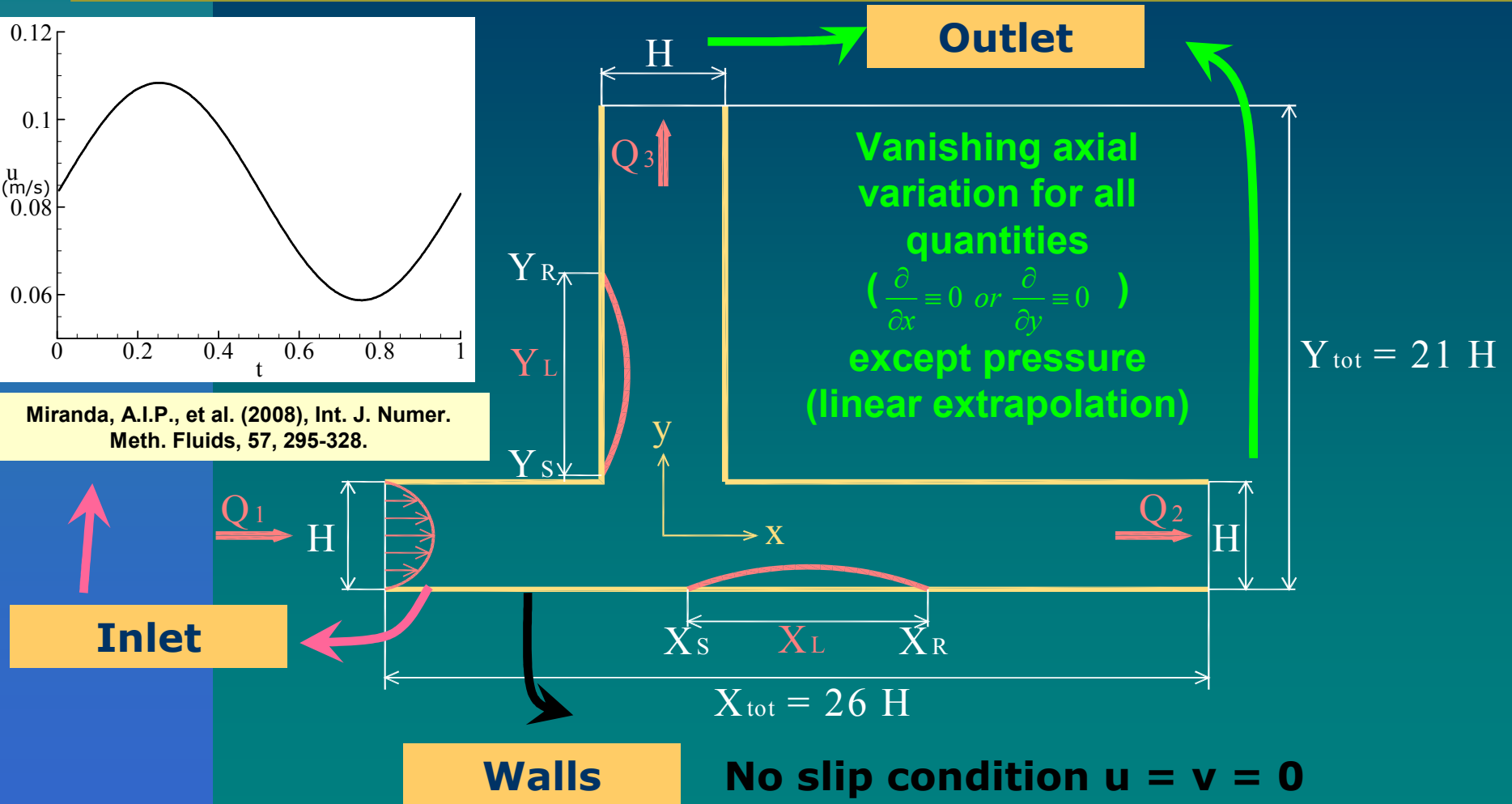


Inlet

# 6 - FLOW GEOMETRY

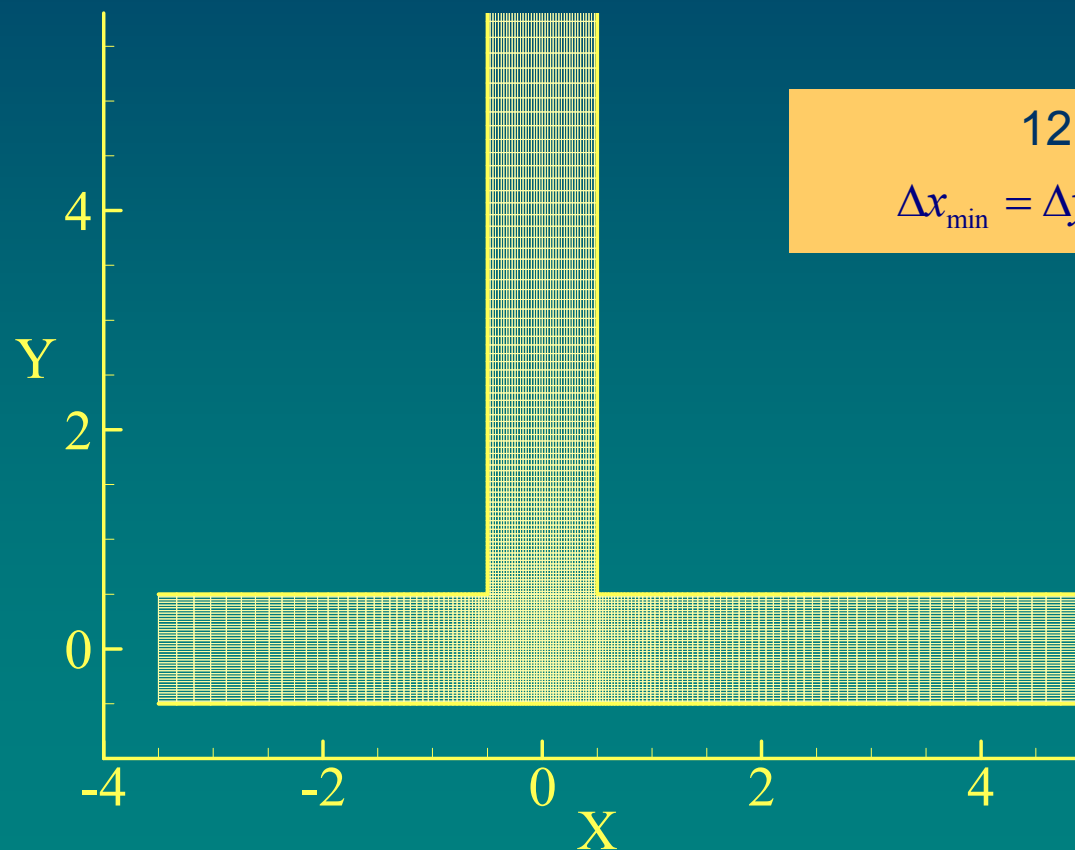


Miranda, A.I.P., et al. (2008), Int. J. Numer. Meth. Fluids, 57, 295-328.



# 7 - MESH

## ■ Orthogonal but non uniform meshes

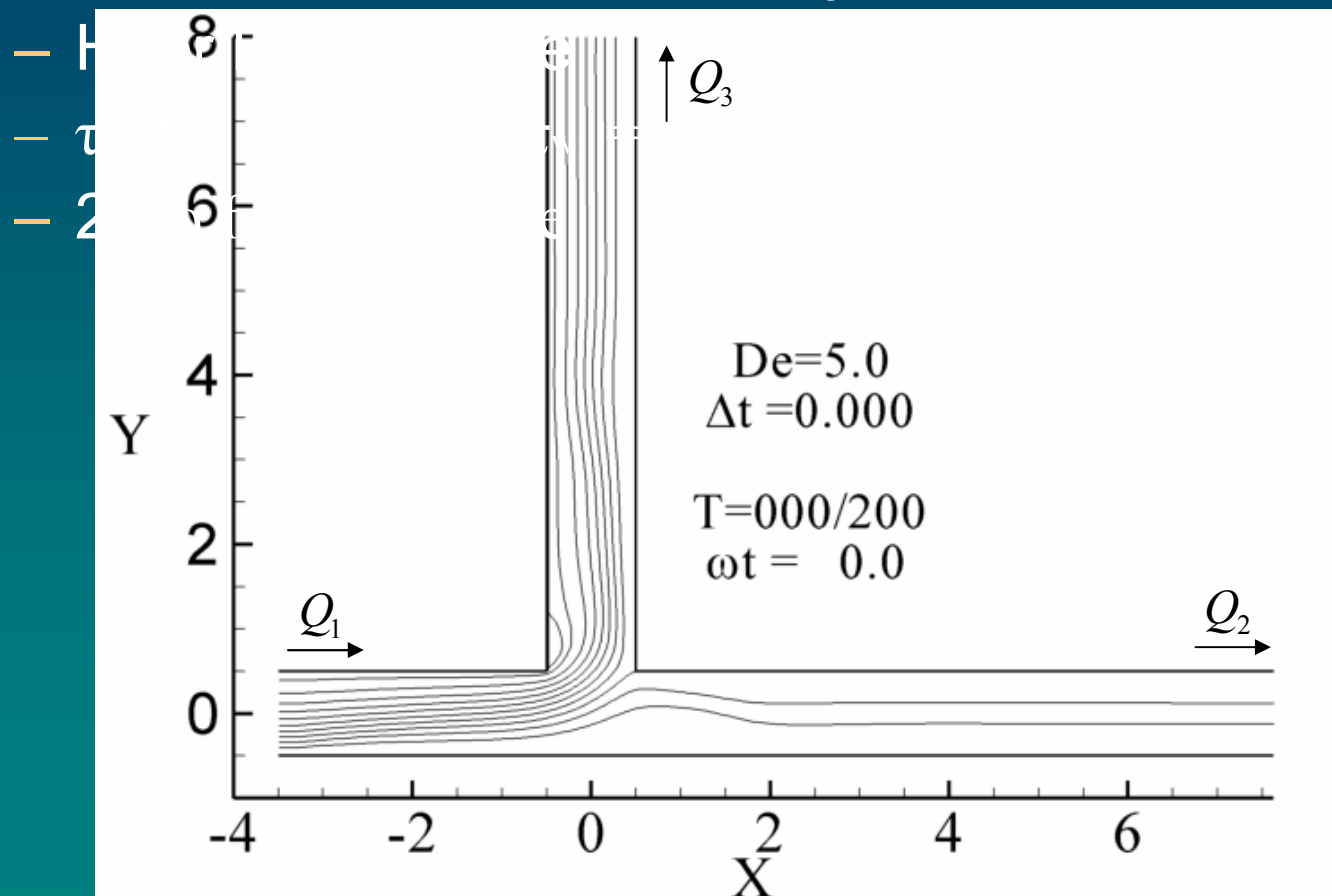


12,800 VC

$$\Delta x_{\min} = \Delta y_{\min} = 2.5 \times 10^{-2}$$

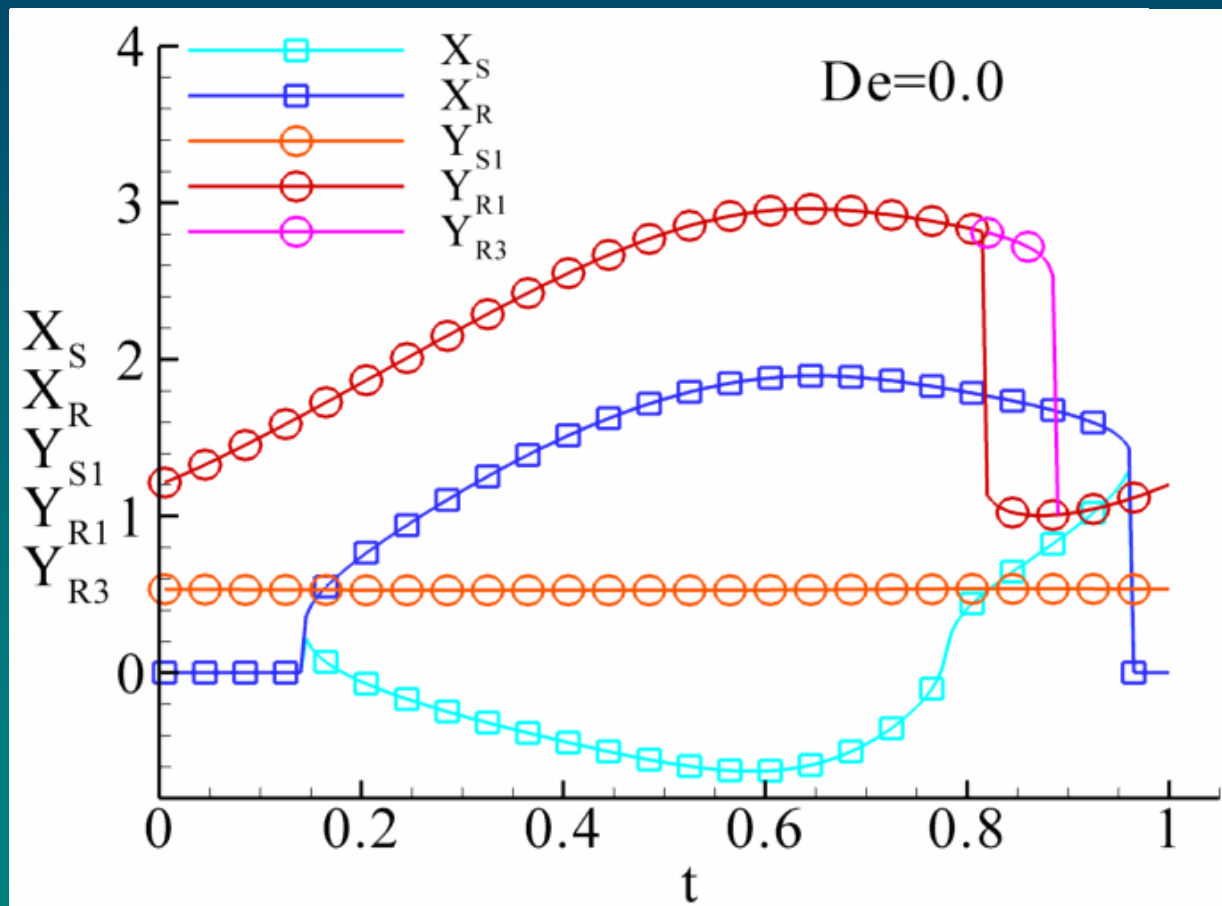
# 8 - RESULTS

## ■ Steady incompressible results ( $\beta = Q_3 / Q_1 = 0.7$ )



## 8 - RESULTS (variation of elasticity)

### ■ Separation and reattachment points ( $\beta = 0.7$ )



residence

– 81.5%

– 75.5%

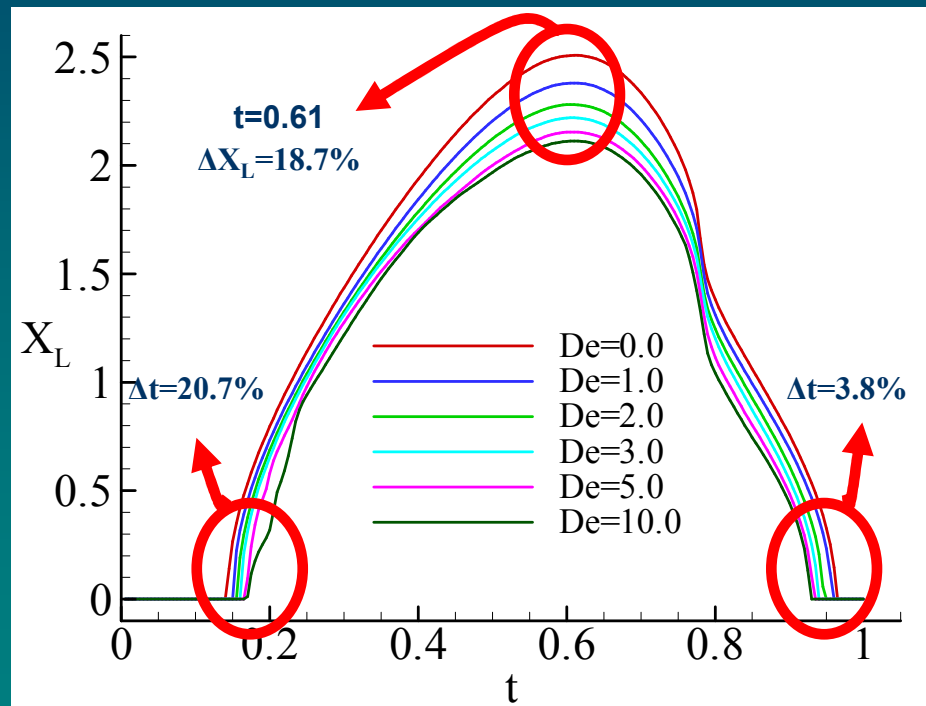
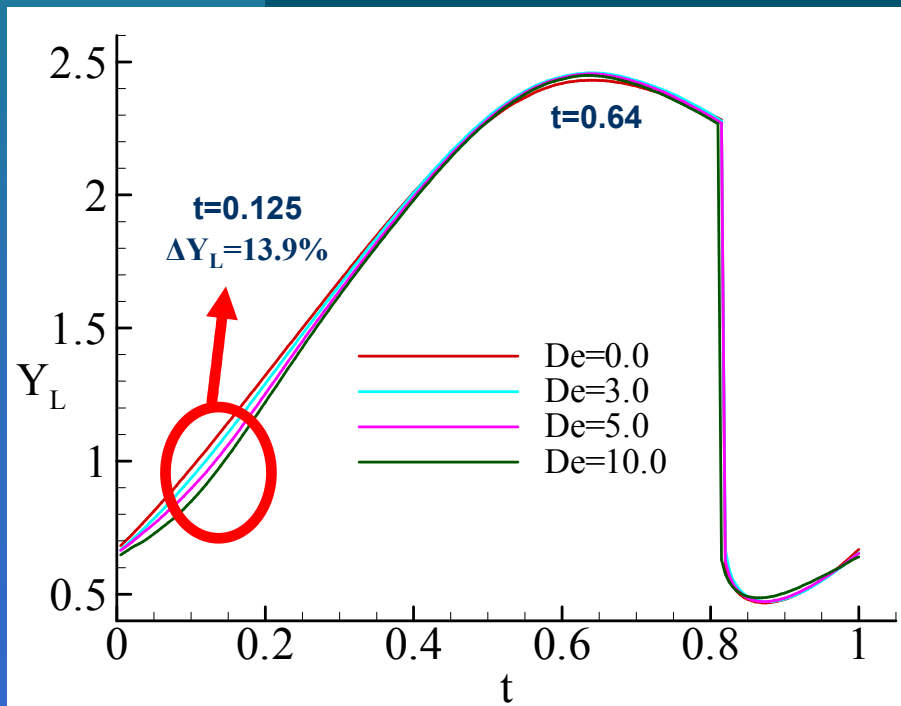
## 8 - RESULTS (variation of elasticity)

- Recirculation lengths ( $\beta = 0.7$ )

**Vertical**

( $E \approx 0.01 - 0.1$ )

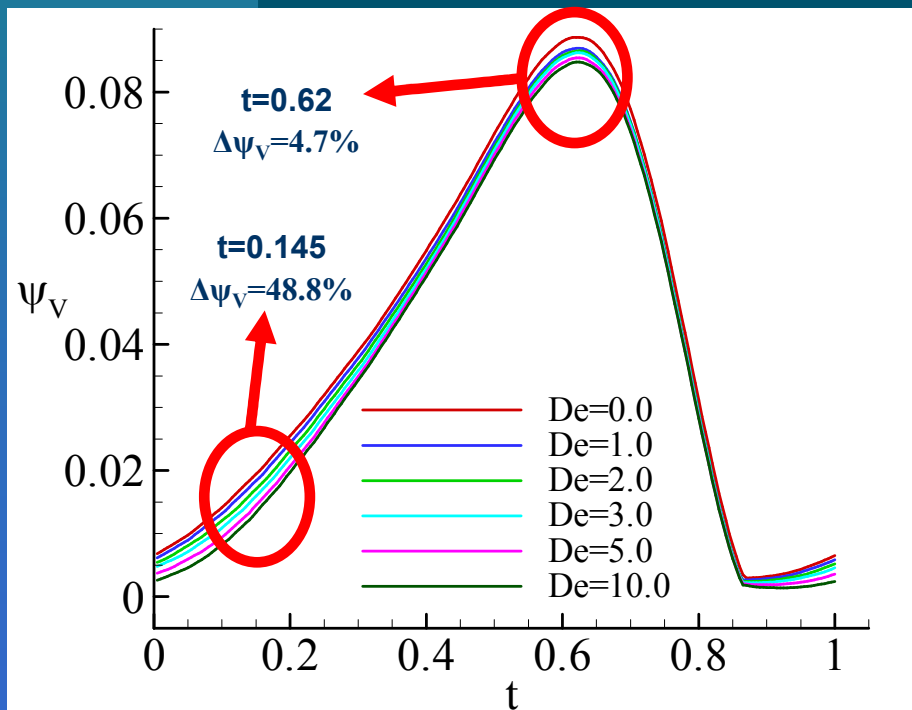
**Horizontal**



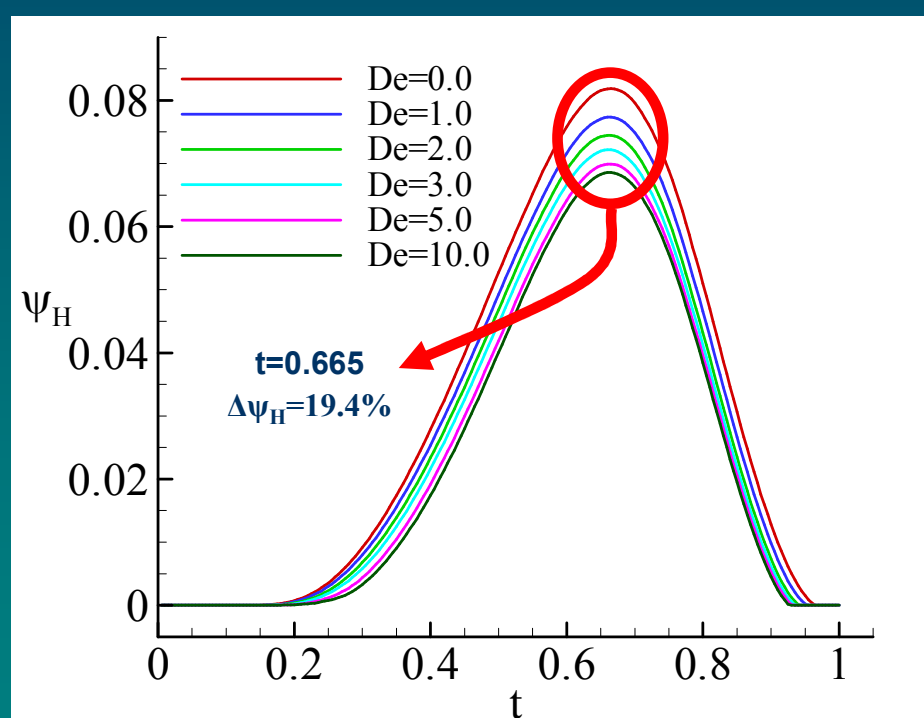
## 8 - RESULTS (variation of elasticity)

- Vortex strength ( $\beta = 0.7$ )

*Vertical*

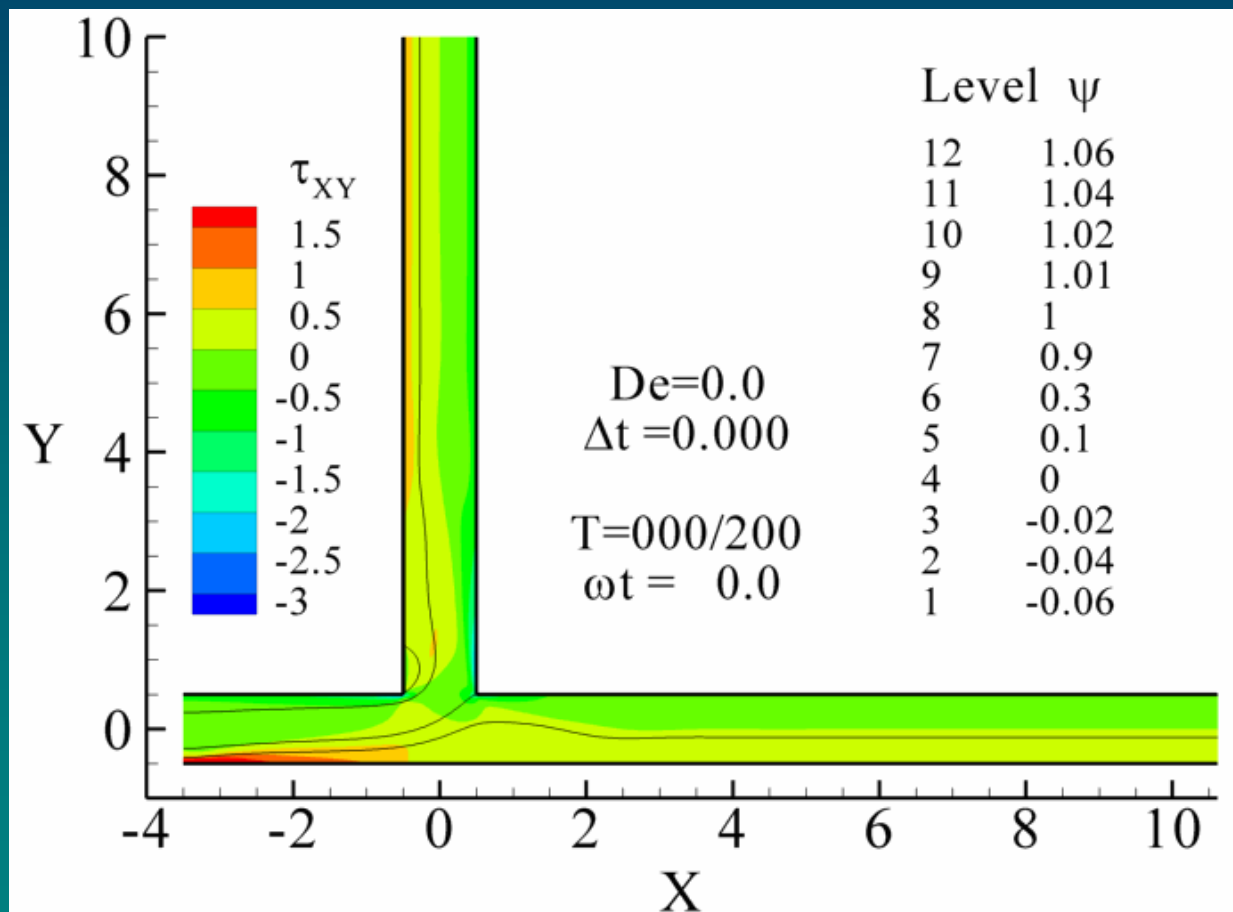


*Horizontal*



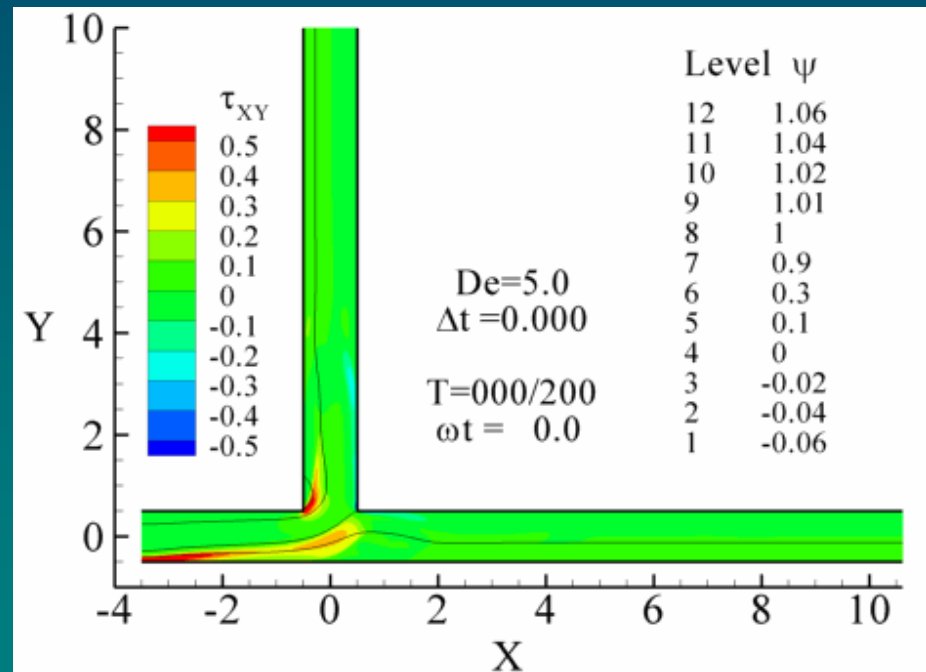
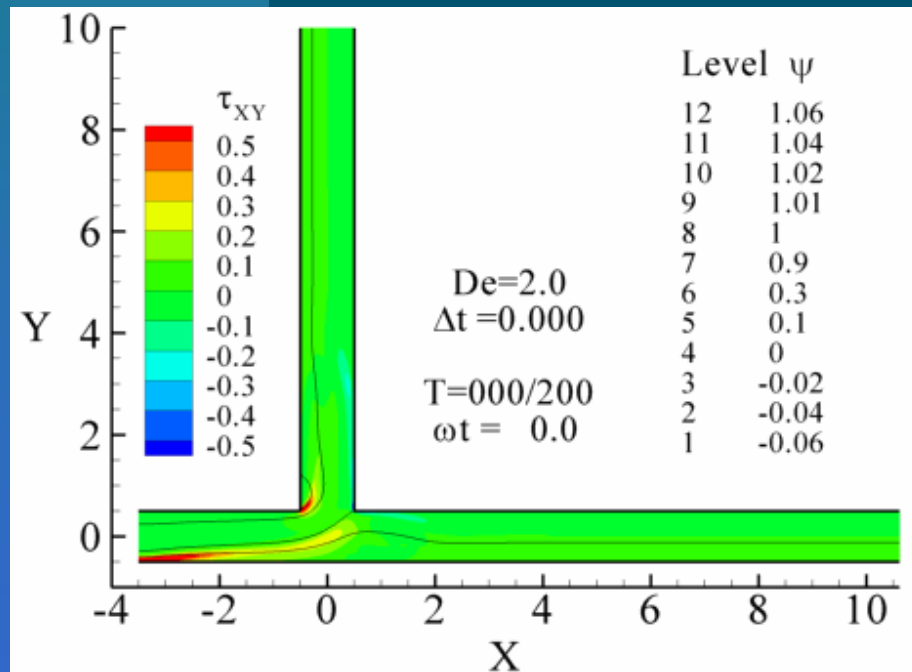
## 8 - RESULTS (variation of elasticity)

### ■ Shear stress field ( $\beta = 0.7$ )



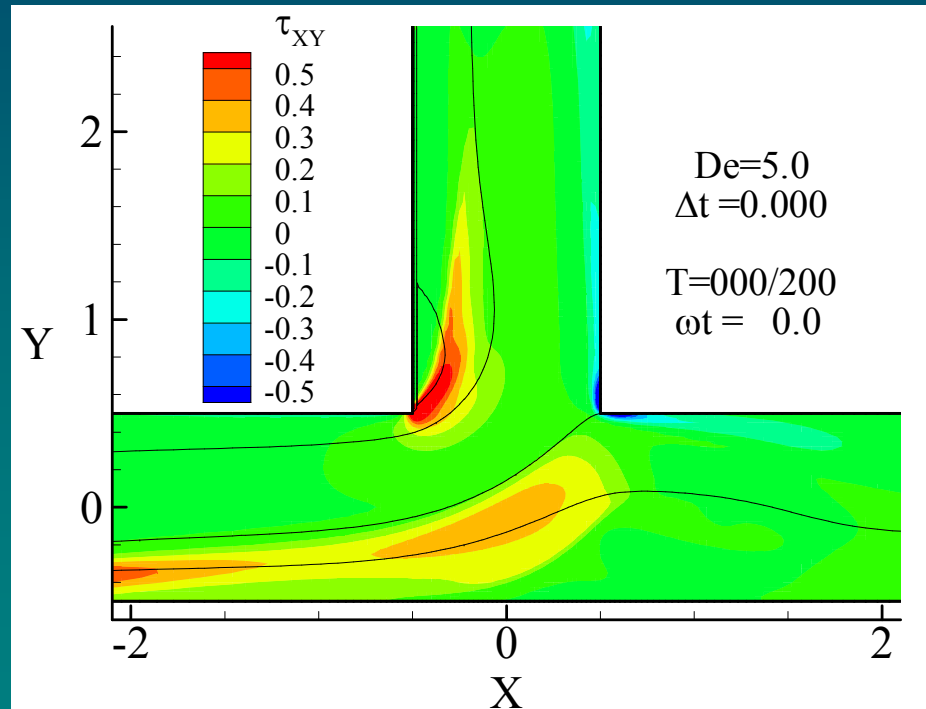
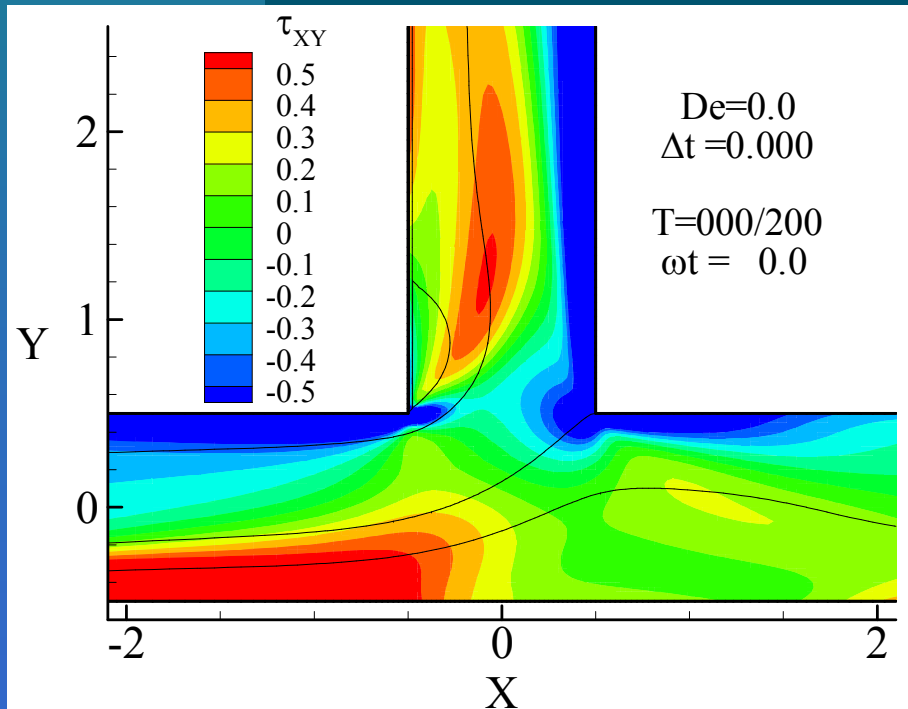
## 8 - RESULTS (variation of elasticity)

- Shear stress field (polymeric components only)



## 8 - RESULTS (variation of elasticity)

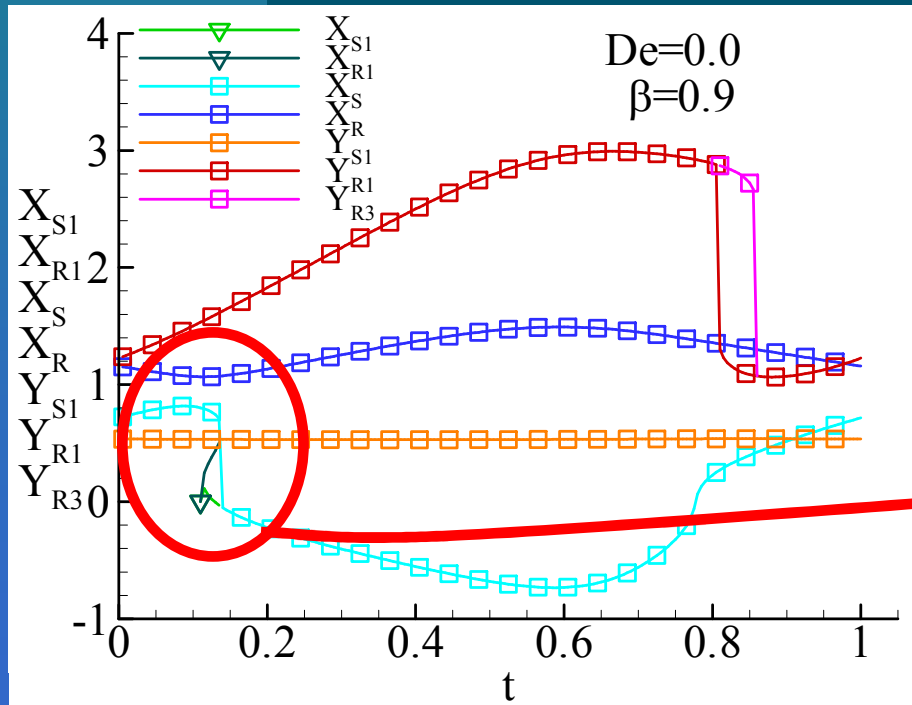
### ■ Shear stress field



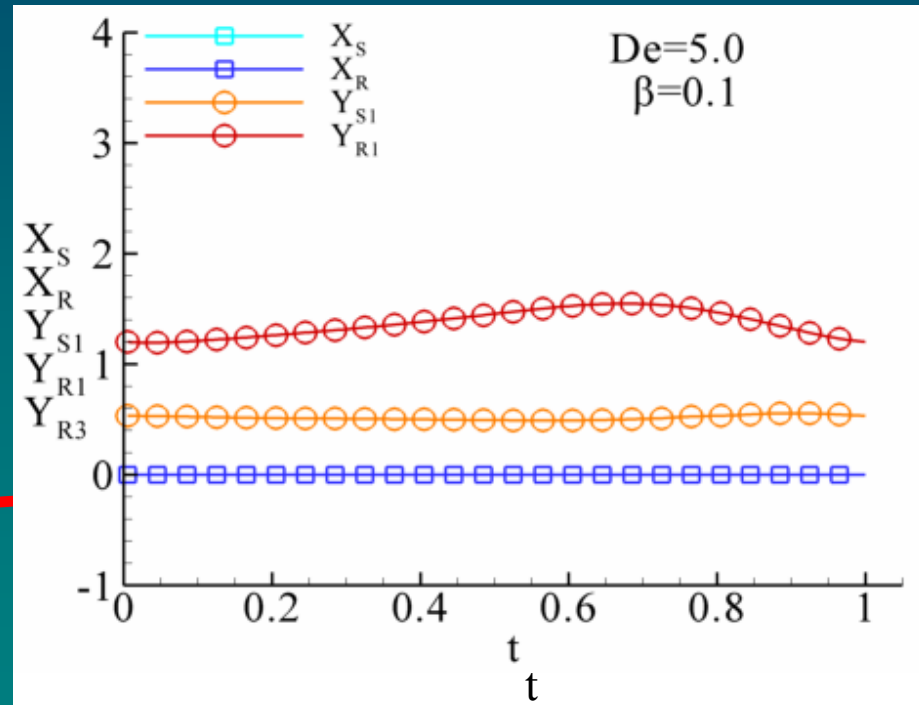
# 9 - RESULTS (variation of extraction ratio)

## ■ Separation and reattachment points

*De=0*

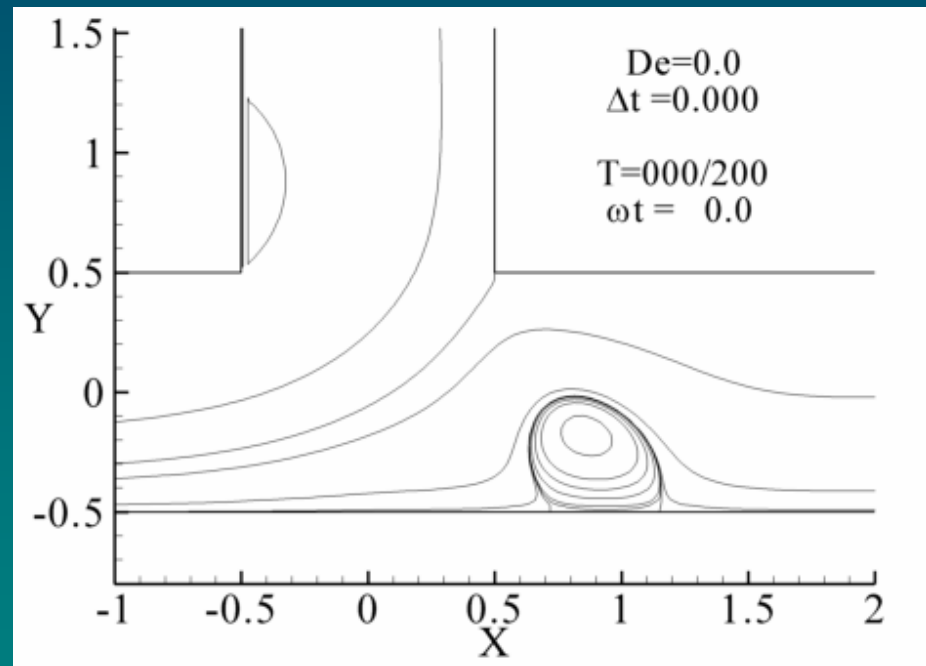
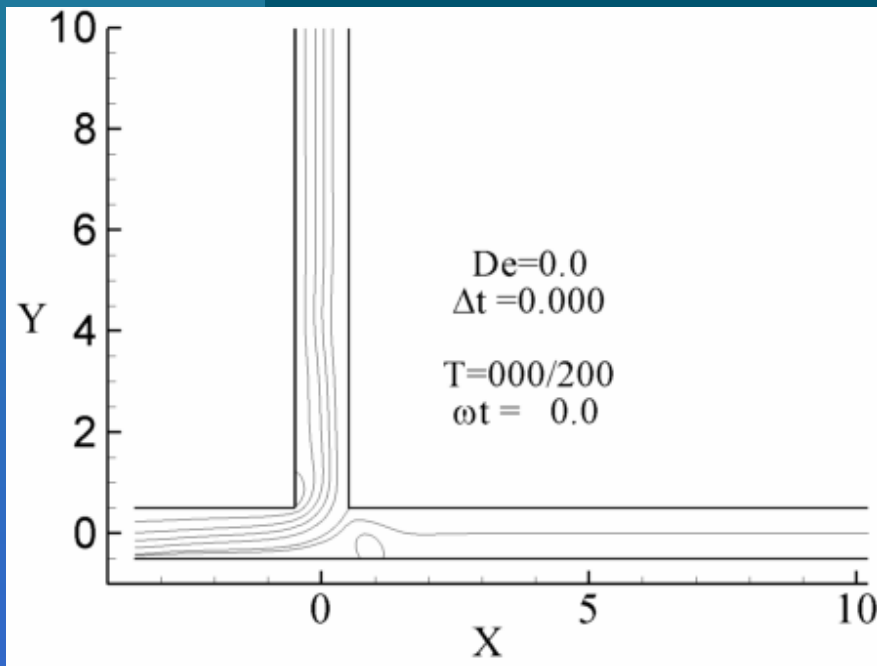


*De=5*



## 9 - RESULTS (variation of extraction ratio)

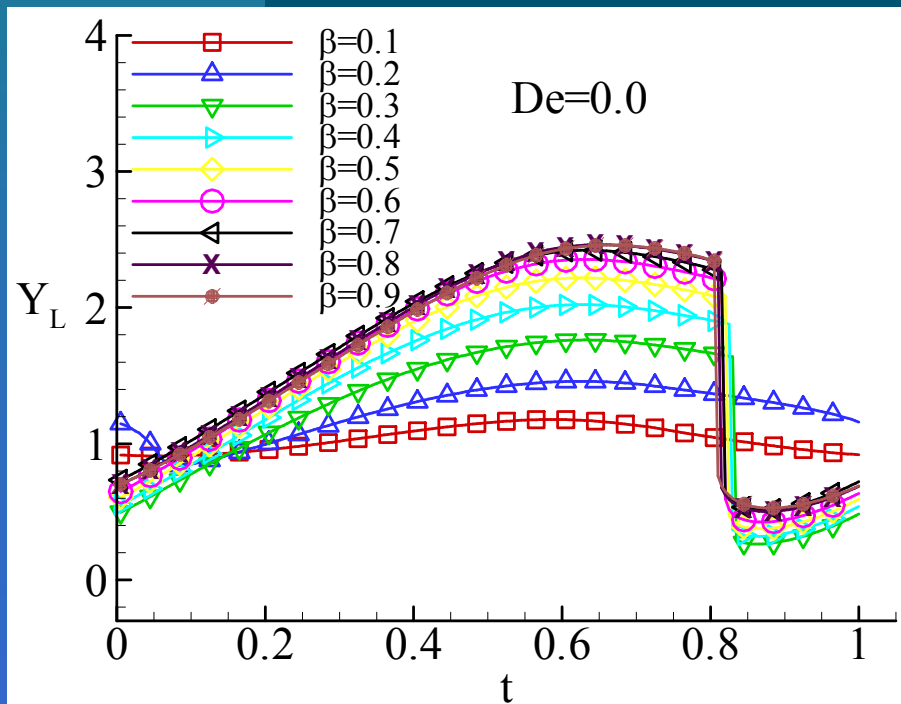
- Streamlines for a cycle ( $\beta = 0.9$ )



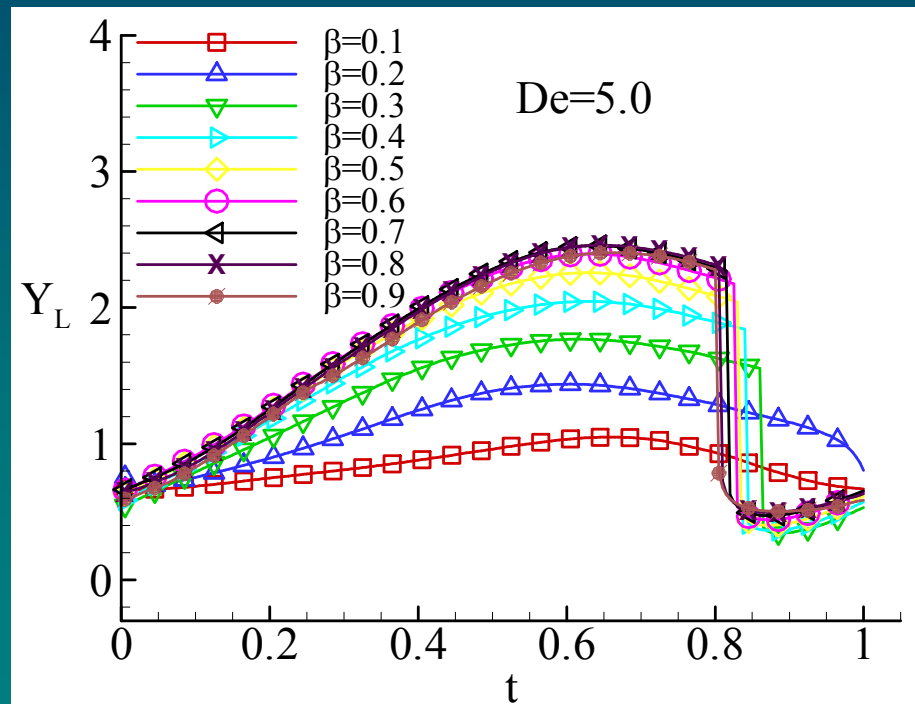
## 9 - RESULTS (variation of extraction ratio)

### ■ Recirculation lengths (Vertical)

$De=0$



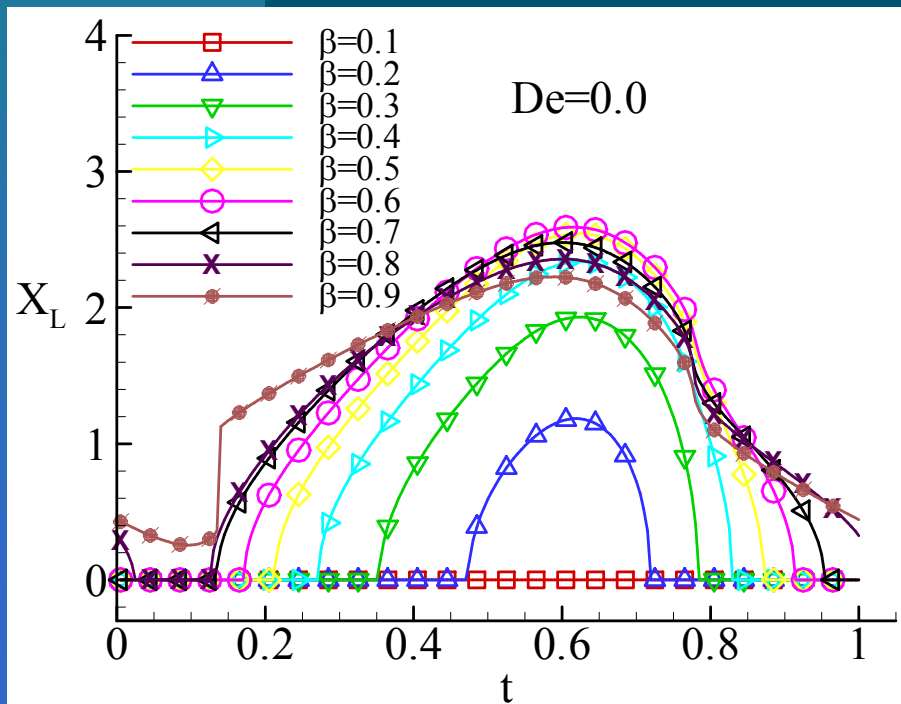
$De=5$



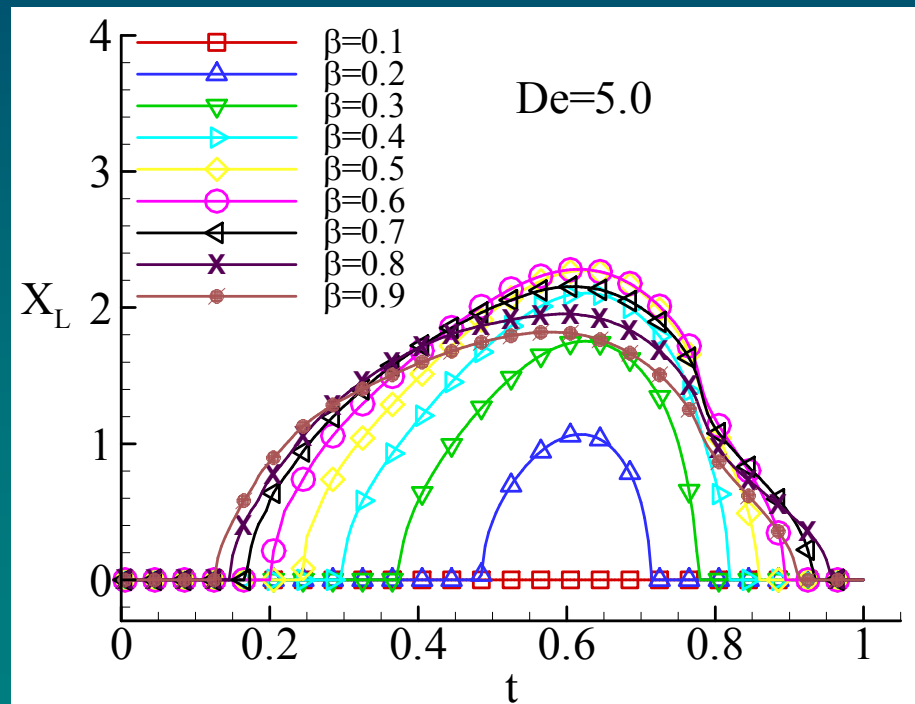
## 9 - RESULTS (variation of extraction ratio)

### ■ Recirculation lengths (Horizontal)

$De=0$



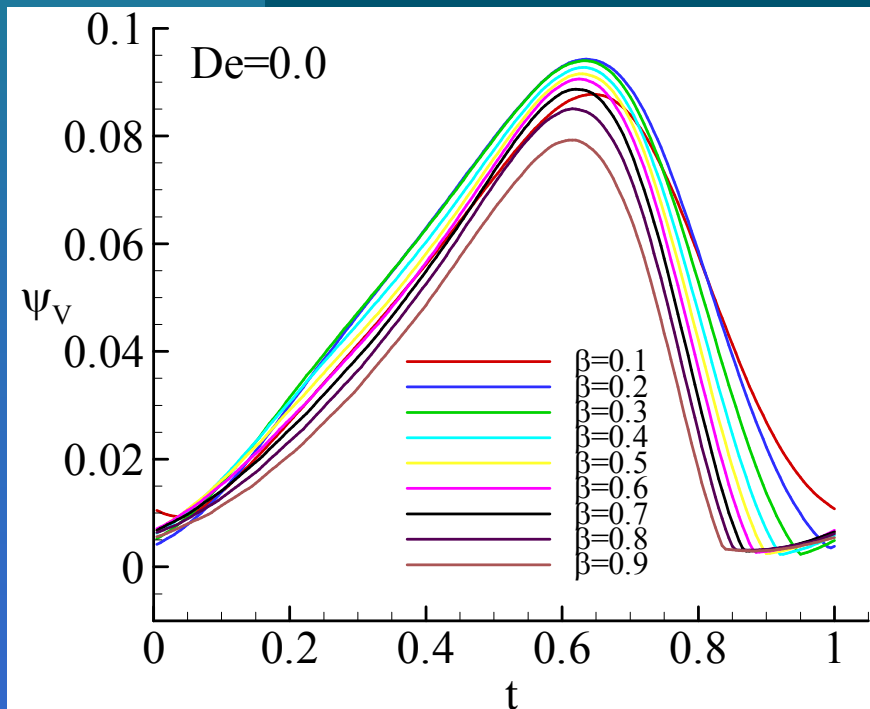
$De=5$



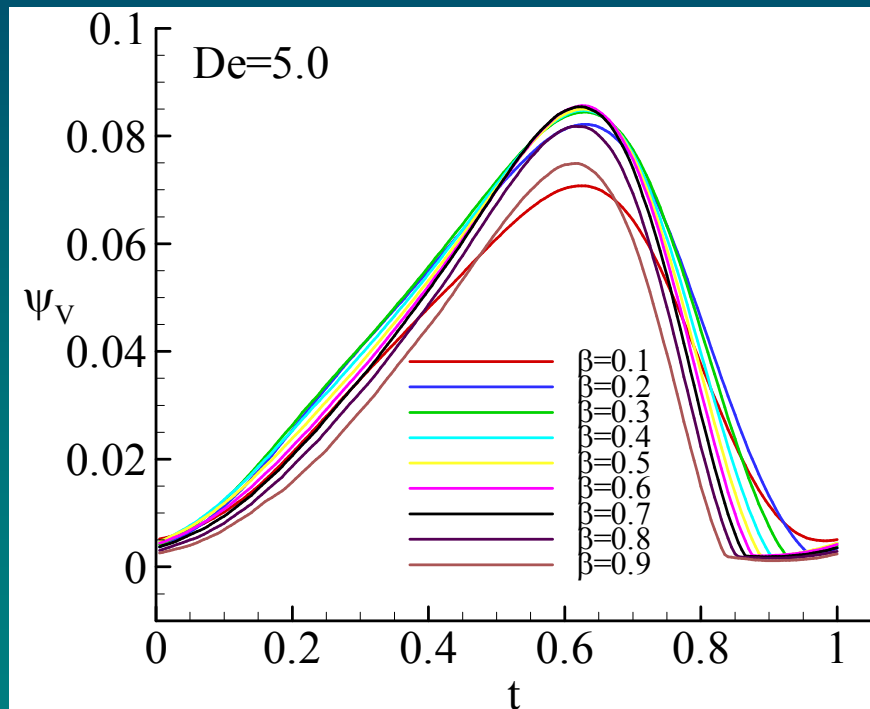
## 9 - RESULTS (variation of extraction ratio)

### ■ Vortex strength (Vertical)

*De=0*



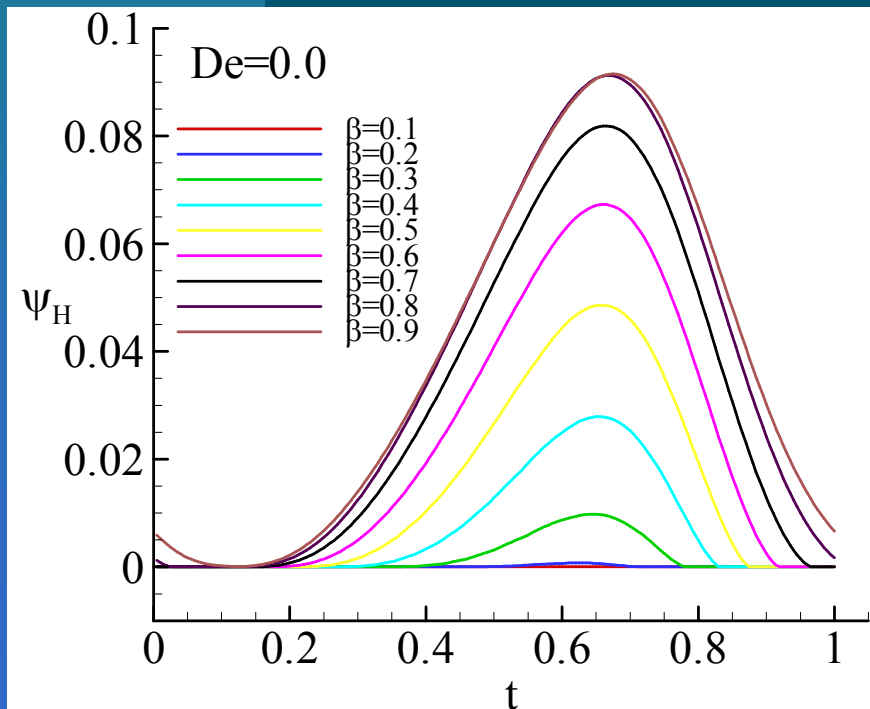
*De=5*



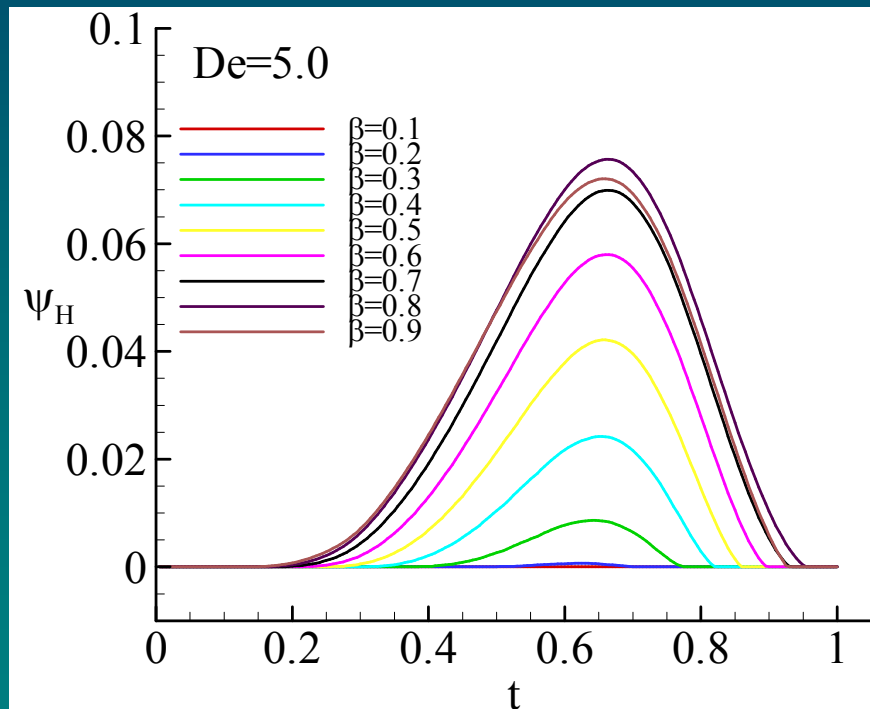
## 9 - RESULTS (variation of extraction ratio)

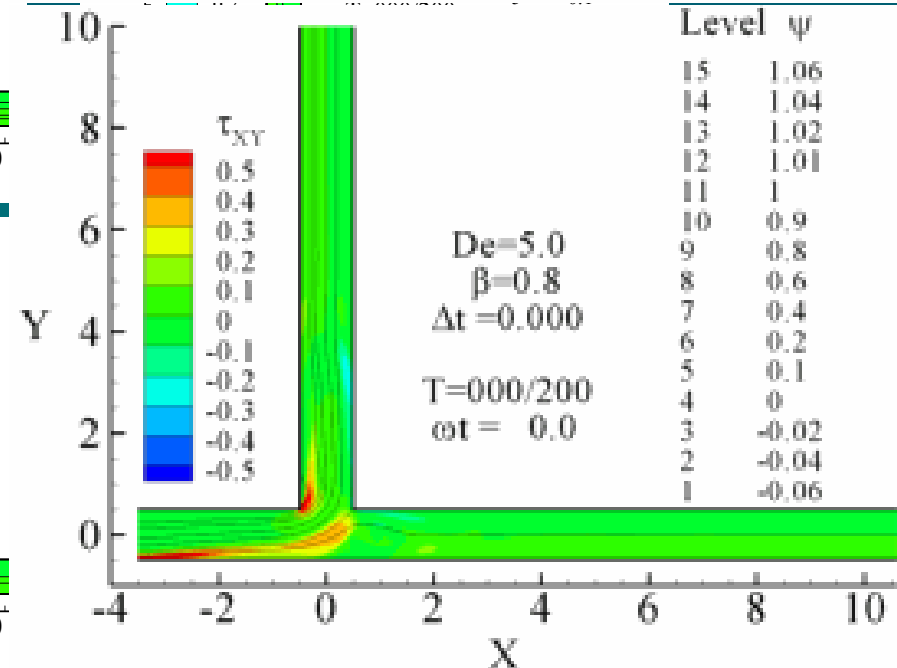
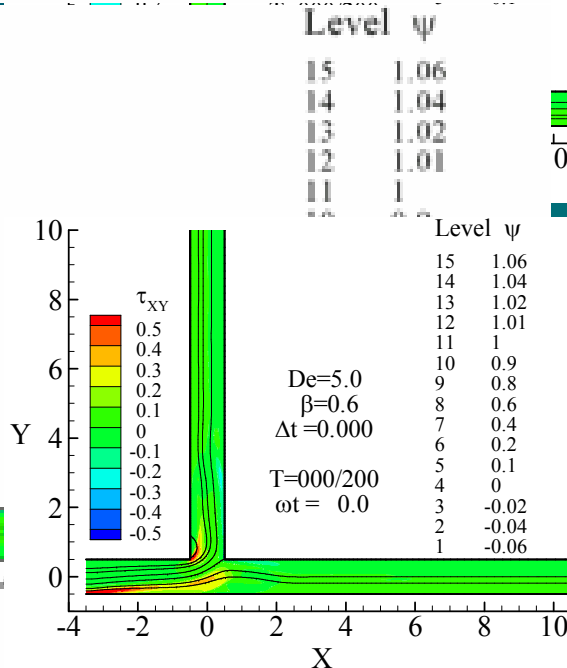
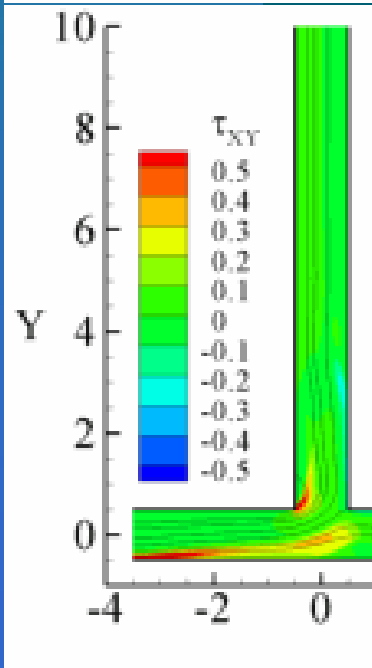
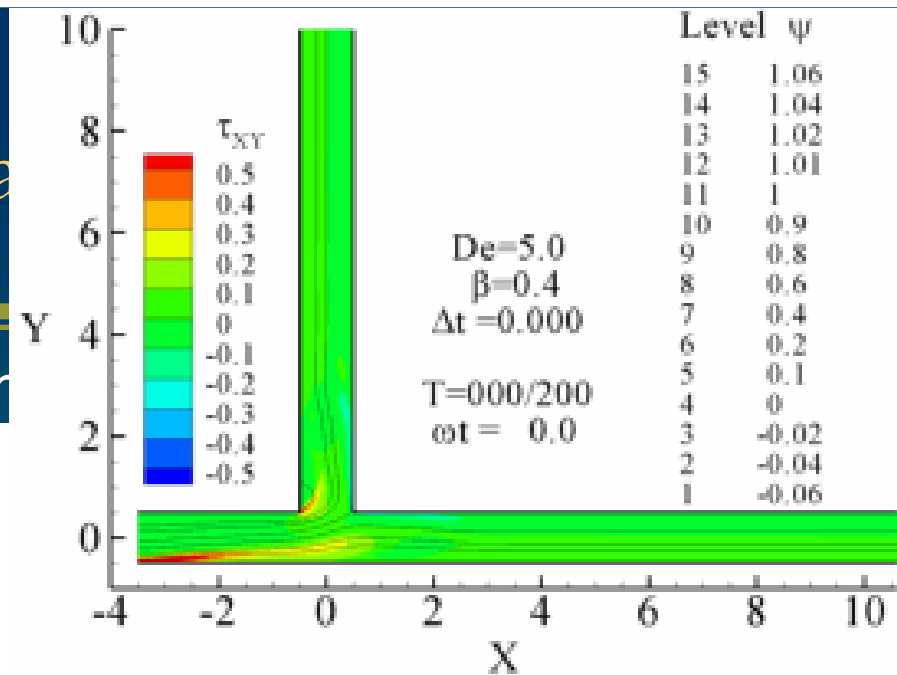
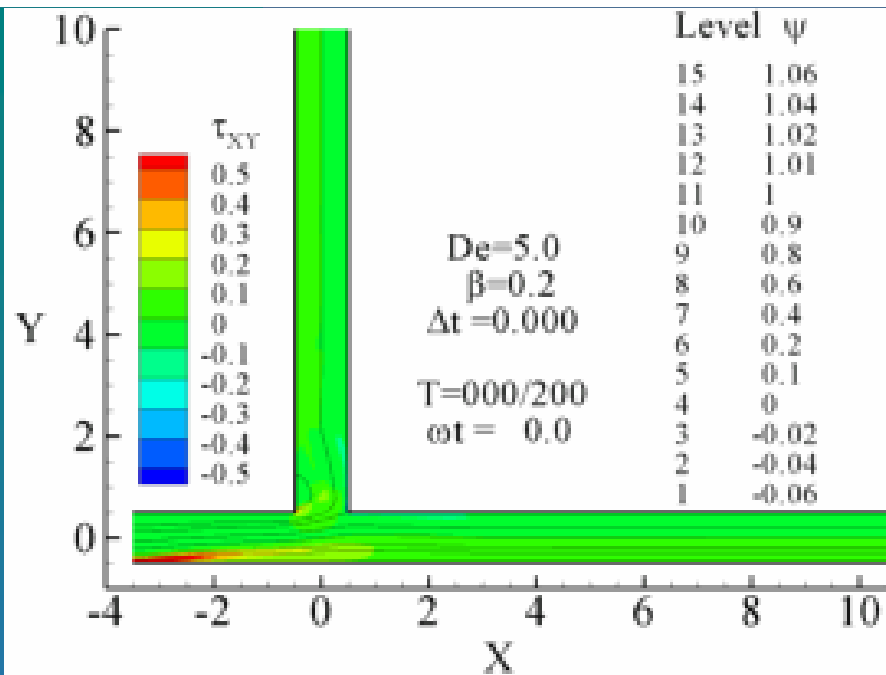
### ■ Vortex strength (Horizontal)

**$De=0$**



**$De=5$**





# 10 - CONCLUSIONS

- Size and intensity of recirculations decrease with  $De$ .
- $Y_L$  increase with  $\beta$ ;  $X_L$  increase with  $\beta$  for  $\beta \leq 0.6$  and decrease for  $\beta > 0.6$ .
- Intensity  $\psi_H$  increase with  $\beta$ .
- Horizontal recirculation not always present: residence interval decrease with  $De$  and increase with  $\beta$ .
- Maximum size and intensity occur after middle of the cycle.

# 10 - CONCLUSIONS

- Polymeric shear stress component increase with  $De$  and  $\beta$ .
- Low stresses inside recirculating zones and high stresses in the re-entrant corners of the bifurcation.
- During the cycle the shear stress field follows the velocity variation, with maximum for  $\omega t \approx 90^\circ$  and minimum values for  $\omega t \approx 270^\circ$ .

# 11 - ACKNOWLEDGEMENTS

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- *University of Beira Interior (Portugal)*



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23/23